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# Modelling hydrolysis: simultaneous versus sequential

# **biodegradation of the hydrolysable fractions**

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#### **Abstract**

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Hydrolysis is considered the limiting step during solid waste anaerobic digestion (including co-digestion of sludge and biosolids). Mechanisms of hydrolysis are mechanistically not well understood with detrimental impact on model predictive capability. The common approach to multiple substrates is to consider simultaneous degradation of the substrates. This may not have the capacity to separate the different kinetics. Sequential degradation of substrates is theoretically supported by microbial capacity and the composite nature of substrates (bioaccessibility concept). However, this has not been experimentally assessed. Sequential chemical fractionation has been successfully used to define inputs for an anaerobic digestion model. In this paper, sequential extractions of organic substrates were evaluated in order to compare both models. By removing each fraction (from the most accessible to the least accessible fraction) from three different substrates, anaerobic incubation tests showed that for physically structured substrates, such as activated sludge and wheat straw, sequential approach could better describe experimental results, while this was less important for homogeneous materials such as pulped fruit. Following this, anaerobic incubation tests were performed on five substrates. Cumulative methane production was modelled by the simultaneous and sequential approaches. Results showed that the sequential model could fit the experimental data for all the substrates whereas simultaneous model did not work for some substrates.

# 45 Keywords

46 ADM1; fractionation; hydrolysis; modelling; model selection; organic matter.

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# List of abbreviations

- 49 ADM1 Anaerobic Digestion Model number one
- 50 ASM Activated Sludge Model

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Biochemical Methane Potential (NmL CH<sub>4</sub>.gVS<sup>-1</sup>)
       BMP
51
      BMP 2.0
                        Biochemical Methane Potential number 2 after acclimation phase (NmL CH<sub>4</sub>.gVS<sup>-1</sup>)
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      DOM
                        Dissolved Organic Matter
                        Chemical Oxygen Demand (g O<sub>2</sub>.g TS<sup>-1</sup>)
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      COD
                        Switching function
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      F_{accessibility_i}
56
      f_X_{RC}xI
                        inert fraction of X_{RC} (% COD)
      f\_X_{RC}\_ch
57
                        carbohydrate fraction of X_{RC} (% COD)
58
      f_X_{RC}pr
                        protein fraction of X_{RC} (% COD)
59
      f_X_{RC}_{li}
                        lipid fraction of X_{RC} (% COD)
60
      f_X_{MC}xI
                        inert fraction of X_{MC} (% COD)
61
                        carbohydrate fraction of X_{MC} (% COD)
      f_X<sub>MC</sub>_ch
62
      f_X_{MC}pr
                        protein fraction of X<sub>MC</sub> (% COD)
      f_X_{MC}li
                        lipid fraction of X_{MC} (% COD)
63
      f_X_{SC}xI
                        inert fraction of X_{SC} (% COD)
64
      f_X<sub>SC</sub>_ch
                        carbohydrate fraction of X_{SC} (% COD)
65
66
      f_X_{SC}pr
                        protein fraction of X_{SC} (% COD)
                        lipid fraction of X_{SC} (% COD)
67
      f_X_{SC_li}
                        inert fraction of X_{NE} (% COD)
68
      f_X_{NE}xI
                        carbohydrate fraction of X_{NE} (% COD)
69
      f_X_{NE}_{ch}
70
      f_X_{NE}_pr
                        protein fraction of X<sub>NE</sub> (% COD)
                        lipid fraction of X_{NE} (% COD)
71
      f_X_{NE}li
                        ADM1 default parameters for disintegration of particular COD into carbohydrates
72
      f_xch_xc
73
      (%COD)
                        ADM1 default parameters for disintegration of particular COD into lipids (%COD)
74
      f_xli_xc
75
                        ADM1 default parameters for disintegration of particular COD into proteins (%COD)
      f_xpr_xc
76
                        ADM1 default parameters for disintegration of particular COD into inerts (%COD)
      f_xi_xc
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      K_{hyd}\_X_{RC}
                        Contois hydrolytic biomass growth rate for X_{RC} hydrolysis (d<sup>-1</sup>)
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Contois hydrolytic biomass growth rate for  $X_{MC}$  hydrolysis (d<sup>-1</sup>)

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 $K_{hyd}\_X_{MC}$ 

79	$K_{hyd}\_X_{SC}$	Contois hydrolytic biomass growth rate for $X_{SC}$ hydrolysis ( $d^{-1}$ )
80	$K_{hyd}\_X_{NE}$	Contois hydrolytic biomass growth rate for $X_{NE}$ hydrolysis ( $d^{-1}$ )
81	$K_{I\_XRC}$	Switching function inhibition parameter for $X_{MC}$ hydrolysis (kg COD. $m^{3}$ )
82	$K_{I\_XMC}$	Switching function inhibition parameter for $X_{SC}$ hydrolysis (kg COD. $m^{-3}$ )
83	$K_{I\_XSC}$	Switching function inhibition parameter for $X_{\text{NE}}$ hydrolysis (kg COD. $m^{\text{-}3}$ )
84	NIRS	Near Infra-Red Spectroscopy
85	VFA	Volatile Fatty Acids
86	VS	Volatile Solids (% dried matter)
87	$X_D$	Dead biomass variable (kg COD. m <sup>-3</sup> )
88	$X_{RC}$	Readily biodegradable fraction (kg COD. m <sup>-3</sup> )
89	$X_{MC}$	Moderately biodegradable fraction (kg COD. m <sup>-3</sup> )
90	$X_{SC}$	Slowly biodegradable fraction (kg COD. m <sup>-3</sup> )
91	$X_{\rm NE}$	Non-extractible fraction (kg COD. m <sup>-3</sup> )

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# 1. Introduction

In mixed substrate biological conversion, hydrolysis is used as the general depolymerisation of substrates into soluble compounds. It is dominated by the actual process hydrolysis – i.e., depolymerisation into monomers by addition of water molecules (Brock and Madigan, 1991). The process is mediated by enzymes, generally in extracellular reactions. In mixed substrate mathematical models, the hydrolysis process must be adequately described to allow predicting spatial and temporal availability of organic substrates for nutrient removal processes (Morgenroth et al., 2002). Hydrolysis is generally considered the limiting step in biodegradation of particulates and solids substrates (Vavilin et al., 2008). Process modelling kinetics is dominated by the limiting steps and hence the hydrolysis model is critical. According to a review made by Morgenroth et al. (2002), hydrolysis and kinetics in wastewater treatment and excess sludge from wastewater treatment applications are not well

understood and first order processes are applied as an aggregate approximation (Eastman and Ferguson, 1981). Hydrolysis refers to all mechanisms that make slowly biodegradable substrate available for microorganism growth (Gujer et al, 1999). In this latter definition, the key word "available" leads to consider three major concepts: bioaccessibility, bioavailability and biodegradability. Hydrolysis is mainly governed by bioaccessibility (Jimenez et al., 2015). Indeed, due to the complex organisation of some organic residues, bioaccessibility defines the access to the molecules. It can depend on physical structure, process duration and hydrolytic activity. Thus, a fraction can become bioavailable by crossing the membrane of the microorganism mediating the degradation (Semple et al., 2007; Aquino et al., 2008). Ultimately, the biodegradable fraction is the bioavailable organic matter consumed by the biomass. Different hydrolysis approaches have been applied in aerobic and anaerobic models. In aerobic process models, the hydrolysis concept has been challenged several times by many authors (Sollfrank and Gujer, 1991; Gujer et al., 1999, Shimizu et al., 1993; Siegrist et al., 1993; Angelidaki et al., 1997, Sperandio and Paul, 2000, Vavilin et al., 2008, Yasui et al., 2008; Mottet et al., 2013; Garcia Gen et al., 2015) since the well-known developed activated sludge models (ASM) (Henze et al., 1987). However, first order processes have been generally applied due to difficulties in identifying higher order models. Multiple (two) particulate biodegradable fractions have been considered not only according to the physical separation process but also to the biological response of the model in a simultaneous degradation way (Ekama and Marais, 1979; Ekama et al., 1986; Henze et al., 1987; Gujer et al., 1999). In this respect, the associated kinetics was based on a surface-limited equation and one biomass. Ekama and Marais (1979) divided the particulate fraction into two biodegradable fractions: a readily biodegradable fraction mainly consisting of soluble organic matter; and a slowly biodegradable fraction consisting of large molecules, colloids and

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particles that have to be hydrolysed before degradation. The distinction between these two 130 131 fractions was also determined by experimental biological response analysis (Ekama et al., 1986; Sperandio and Paul, 2000). 132 As regards anaerobic process models such as the Anaerobic Digestion Model No. 1 (ADM1, 133 Batstone et al., 2002), one biodegradable fraction was initially considered. Then, this 134 biodegradable fraction is split into biochemical fractions (i.e. carbohydrates, lipids, proteins 135 and inert) after a disintegration process (i.e., a mix of sequential and simultaneous). This 136 approach was not supported by experiments, and was purely conceptual, and has been 137 criticised (Batstone et al., 2015). Other previous studies (see, for instance, Shimizu et al., 138 1993; Siegrist et al., 1993; Angelidaki et al., 1997) have generally applied first order kinetics. 139 The common approach in the event of inadequate model performance is: (i) to increase the 140 number of hydrolysable fractions (Sollfrank and Gujer, 1991, Orhon et al., 1998; Sperandio 141 142 and Paul, 2000; Yasui et al., 2008; Mottet et al., 2013; Garcia-Gen et al., 2015); (ii) to replace the first order kinetics by surface limitation equations (i.e. Contois equation, Vavilin et al., 143 144 2008; Mottet et al., 2013), or (iii) to include a particle size distribution model (Dimock et al., 2006; Sanders et al., 2000; Yasui et al., 2008); (iv) to differentiate non-active and active 145 hydrolytic bacteria in particles colonization (Ginestet et al., 2001; Benneouala et al., 2017). 146 In the studies considering several hydrolysable fractions, some authors considered 147 simultaneous degradation (Sollfrank and Gujer, 1991; Lagarde et al., 2005; Orhon et al., 148 1998; Mottet et al., 2013; Garcia-Gen et al., 2015; Kouas et al., 2017) and others sequential 149 degradation (Bjerre, 1996; Confer and Logan, 1997; Lagarde et al., 2005; Spérandio and 150 Paul., 2000, Yasui et al., 2008). These approaches are inconsistent mechanistically and in 151 basic kinetic response. A key challenge is to determine experiments to identify the most 152 153 appropriate approach.

Recently, a promising methodology for organic matter characterisation has been successfully developed to describe the organic matter bioaccessibility and bioavailability of organic residues (Muller et al., 2014; Jimenez et al., 2015). Jimenez et al. (2014) showed that bioaccessibility could be determined for wastewater treatment sludge using sequential extractions to characterize the organic matter accessibility. This fractionation method was subsequently used to determine new input variables of a modified ADM1 model in order to predict biogas performance and digestate quality of an anaerobic digester fed with sludge (Jimenez et al., 2015a). Since the method is a sequential chemical procedure, it is possible to isolate and consider each fraction separately and to perform biological tests on them to evaluate simultaneous or sequential behaviour. In this paper, the use of the new fractionation methodology, describing bioaccessibility, was applied on several substrates and their respective fractions in anaerobic incubation tests. The results of the fractionation methodology were used as input variables of an anaerobic digestion model for the treatment of different organic wastes related to the two hypotheses: simultaneous and sequential concepts. Finally, the objective of this paper was to challenge the classical simultaneous concept of multi-substrates hydrolysis experimentally (i) by using the bioaccessibility characterization and anaerobic incubation tests and (ii) by comparing simulation results obtained by simultaneous approach modelling and sequential approach modelling.

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# 2. Material and methods

## 2.1.Accessibility characterization

The accessibility characterization methodology was based on sequential chemical extractions that can be used as indicators to describe the biochemical molecules of a substrate. Indeed,

Jimenez et al. (2015a) showed that each fraction, from the most to the least accessible one, is composed of different kinds of molecules associated to the extraction nature which impact the biodegradability. The characterisation methodology used in this study is detailed in (Jimenez et al., 2014, 2015b) and has been optimised in order to fractionate the substrate within 2 days instead of 5 days. The main optimisation was obtained by pooling the first two extractions into only one, corresponding to the most accessible fractions, which were biodegraded with same kinetics as shown by (Jimenez et al., 2014).

First, a liquid/solid phase separation was performed by sample centrifugation (18600g, 20 minutes,  $4^{\circ}$ C) and the supernatant was filtered at 0.45  $\mu$ m. The recovered filtered supernatant fraction was considered as the first fraction named Dissolved Organic Matter (DOM). It was considered as the most available fraction. The fraction retained by the filter is measured, but is not normally considered further, as it represents a negligible quantity of COD. The solid pellet was dried and milled (1mm) and sequential chemical extractions (30 mL) were performed on 0.5 g of this dried pellet.

Based on Jimenez et al. (2014, 2015a,b), three fractions were considered in this study and were obtained by performing sequential chemical extractions, as follows:

- The readily hydrolysable fraction ( $X_{RC}$ ) was obtained from supernatant of a saline basic extraction (pellet suspended in 30 mL of 10 mM NaCl and 10 mM NaOH twice) and centrifuged for 15min, at 30°C and 300 rpm.
- The moderately hydrolysable fraction ( $X_{MC}$ ) was obtained from the supernatant of 4 sequential basic extractions (30 mL of 0.1M NaOH) of the remaining pellet for 1 h, at 30°C and 300 rpm.
- The slowly hydrolysable fraction ( $X_{SC}$ ) was obtained from the supernatant of 2 sequential strong acid extractions (25 mL 72% w/v  $H_2SO_4$ ) of the remaining pellet for 3 h, at 30°C and 300 rpm.

• The non-extractable fraction  $(X_{NE})$  was obtained by subtraction.

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2.2. Analysis on the chemical sequential extractions 206 The Chemical Oxygen Demand (COD) was measured in duplicate using Aqualytic kits (0-207 1500 mg O<sub>2</sub>.L<sup>-1</sup>) on substrates and extracts. Indeed, the analysis of the freeze-dried and milled 208 209 (1 mm) sample was performed on a solution of 1g.TS.L<sup>-1</sup>). At each extraction step, the insoluble fraction was recovered, dried and milled at 1 mm. The 210 BMP values of each remaining fraction were obtained using an innovative and rapid 211 FlashBMP® method developed by Ondalys (Lesteur et al., 2011). This method is based on 212 Near InfraRed Spectroscopy (NIRS) applied to more than 600 types of wastes (agro-industrial 213 214 waste, green waste, energy crops, municipal solid waste, sludge and digestates) for which classical BMP tests were performed according to Angelidaki and Sanders (2004). Samples 215 were freeze-dried and milled at 1 mm before NIRS acquisition. Spectra were measured using 216 a BUCHI NIRFlex N-500 (Buchi, Switzerland), with add-on vials. Results are expressed in 217 mL CH<sub>4</sub>.gVS<sup>-1</sup>. The biodegradability of each fraction can be then obtained by converting the 218 results into in mL CH<sub>4</sub>.gCOD<sup>-1</sup> and divided by 350 mL CH<sub>4</sub>.gCOD<sup>-1</sup>, the theoretical yield 219 (Angelidaki et al., 2004). 220 Proteins and carbohydrates of each fraction were analysed respectively by the Lowry method 221 (Lowry et al., 1951) and the Dubois method (Dubois et al., 1956). Lipids were analysed as 222 heptane extractable material by gravimetry. 1 g of freeze-dried and milled sample was 223 extracted with 25 mL of hot and pressurized heptane using an extra-Accelerated Solvent 224 Extractor ASE 200 (Thermo Fisher Scientific®, Sunnyvale, California 94085 USA). The 225 extracted solution was collected in a 60 mL glass vial. The heptane was evaporated under a N<sub>2</sub> 226 flow. The quantity of extracted fatty matter was measured once the remaining sample was 227 dried at 105°C for 2 hours. 228

#### 2.3. Anaerobic incubation tests:

In addition to the FlashBMP measurements, two types of anaerobic incubation tests were used in the study: (i) a classical biochemical methane potential (BMP) to assess the maximum anaerobic biodegradability of a substrate, in optimal conditions for a characterization objective, and (ii) a successive batch anaerobic reactor to acclimate the microorganisms and simulate the real digester performances for modelling objective.

#### Classical BMP test

- Three model substrates of different composition were selected: wheat straw (i.e. lignocellulosic substrate where biodegradable material is protected by an external layer of recalcitrant tissue), apple (carbohydrates substrate) and wastewater treatment sludge from an activated sludge plant (retention time of 20 days). Wastewater treatment sludge was selected to be representative of microorganism compounds, rich in proteins and exo-polymeric susbtances organised in flocs (Jimenez et al., 2014). The three substrates were fractionated as described by the Jimenez et al. (2015a,b) protocol. At each step of the chemical extraction protocol, the recovered pellet after centrifugation was incubated under anaerobic conditions, with the same substrate COD concentration as described in Jimenez et al. (2014). Three samples were considered:
  - the initial substrate (wheat straw, apple or wastewater treatment sludge);
  - the pellet recovered after the first extraction (two saline extractions) and after centrifugation;
    - the pellet recovered after the first two extractions (two saline extractions and four basic extractions) and after centrifugation. .

The experimental conditions were those described by Angelidaki et al. (2004) for the biochemical methane potential (BMP) assessment, in 500 mL bottles. The substrate/inoculum ratios were 0.5 g VS.g VS<sup>-1</sup>. These tests were named BMP tests in this study.

## • Successive batch tests

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Torrijos et al. (2015) developed a new protocol to assess the BMP value. In order to be closer to the real conditions of a continuously fed digester, successive batch tests were conducted to achieve inoculum acclimation in a 6-L lab-scale reactor. Once the methane production kinetics obtained was stable, the microorganisms were considered acclimated to the substrate.. A last feed was then added. These final data were used for modelling purposes. The reactor was magnetically stirred. A temperature of 35°C was maintained in the reactors by a double wall fed with 35°C water from a water bath. The biogas production was measured on-line by Milligascounter MGC-1 flow meters (Ritter® gas meters) with a 4-20 mA output. Gas composition was measured using a Shimadzu GC 8 chromatography associated with a Shimadzu GC 3A integrator. The carrier gas was argon. The organic load of each batch was 1 g VS.L<sup>-1</sup> and the substrate/inoculum ratios were 0.08 g VS.g VS<sup>-1</sup>. In this study, successive batch tests were obtained from several experiments of anaerobic digestion of the following organic residues: wheat straw, apple, carrot, potatoes, lettuce, cauliflower and wastewater treatment sludge. Eight fed batch tests were operated before reaching the acclimation of the tested substrates. Wastewater treatment sludge kinetics data were provided by the same test but only after 30 days of batch feeding before data collection (Jimenez et al. 2015a data). Four cumulated methane production curves were obtained over four feed cycles to strengthen the model calibration.

# 2.4. Definition of simultaneous and sequential concepts

Regarding hydrolysis and biodegradability concepts, the bioaccessibility of a molecule needs to be considered. Indeed, according to Jimenez et al. (2015b), an organic fraction is defined as

"bioaccessible" if, at some point, microorganisms have access to it. This depends on several factors, such as process duration, hydrolytic activity of the microorganisms, or the pretreatments applied. Once bioaccessible, a fraction is biodegradable if it is able to cross the membrane of the microorganism. Semple et al. (2011) defined a minimum size of 10 kDa for molecules to cross the membrane. Therefore, hydrolysis aims at reducing the size of the molecule. Enzymatic potential of the microorganisms and the physical characteristics of the molecule (i.e. size) govern its bioaccessibility. To make a molecule bioavailable, simultaneous versus sequential hydrolysis concepts are two different ways considered in hydrolysis modelling. Figure 1 gives a schematic overview of these definitions. In the simultaneous concept, all fractions  $X_{RC}$ ,  $X_{MC}$  and the least degradable fractions  $X_{SC}+X_{NE}$  are degraded simultaneously. As the most readily degradable fractions are consumed, the overall hydrolysis rate reduces, and hence the degradation kinetics parameters for each fraction are dominated by the slowest degradable fraction. Concerning the sequential concept, the most accessible fraction (i.e.  $X_{RC}$ ) is first degraded. This fraction acts as a protection layer and limits the next accessible fraction (i.e. X<sub>MC</sub>) degradation. Similarly  $X_{MC}$  fraction limits the least accessible fractions (i.e.  $X_{SC}+X_{NE}$ ) degradation. Consequently, during the first period of degradation, X<sub>RC</sub> is the only fraction consumed, before the degradation of  $X_{MC}$  and the degradation of  $X_{SC}+X_{NE}$ .

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# 2.5.Model implementation

The input variables of the Anaerobic Digestion model  $n^{\circ}1$  (ADM1, Batstone et al., 2002) were replaced by outputs from the fractionation method, i.e. readily hydrolysable fraction  $X_{RC}$ , moderately hydrolysable fraction  $X_{MC}$ , slowly hydrolysable fraction  $X_{SC}$  and non-extractable fraction  $X_{NE}$ . Each fraction contains proteins, lipids and carbohydrates as in ADM1. The fractions are degradable according to the parameters  $f_{X_{RC}}xI$ ,  $f_{X_{MC}}xI$ ,

303 sum of unbiodegradable fraction (i.e. inert in ADM1), carbohydrates, lipids and proteins 304 ratios has to be equal to 1. Figure 2 shows a schematic overview of the modified model. ADM1 processes were used as 305 in Batstone et al., (2002). Hydrolysis kinetics was replaced by the Contois (saturation) 306 kinetics model (Vavilin et al., 2008; Mottet et al., 2013), see equation 1. The death-307 308 regeneration concept was kept but a new variable was introduced as the dead biomass fraction (X<sub>D</sub>) which was hydrolysed into proteins, carbohydrates, lipids and inerts using parameters 309 from Batstone et al., (2002) (i.e. f\_xpr\_xc, f\_xch\_xc, f\_xli\_xc and f\_xi\_xc). Indeed, the dead 310 311 biomass was regenerated into the substrate fraction X<sub>C</sub> in the initial ADM1 model. In the modified model, four particulate COD fractions were considered. The substrates fractions and 312 the regenerated dead biomass were split to avoid confusion in their respective biochemical 313 314 repartition. A "switching" function was introduced in order to simulate sequential hydrolysis which 315 switched off one process while switching on the next (Equations 2 to 4). This function was 316 added to each hydrolysis process by introducing three parameters K<sub>I</sub>\_X<sub>RC</sub>, K<sub>L</sub>X<sub>MC</sub> and 317 K<sub>I</sub>\_X<sub>SC</sub>, as limiting fractions concentrations. In the sequential hydrolysis model, the switching 318 319 function was below 1. Indeed, it represented a limitation for the next accessible fraction, depending on the K<sub>L</sub>X parameters values. No limitation occurs in the simultaneous case 320 where switching function parameters values (K<sub>L</sub>X<sub>RC</sub>, K<sub>L</sub>X<sub>MC</sub> and K<sub>L</sub>X<sub>SC</sub>) were considered 321 much higher than the fractions concentrations values. 322

f\_X<sub>SC\_x</sub>I, f\_X<sub>NE\_x</sub>I, where (1-f\_X<sub>I</sub>) is the biodegradable fraction of each component. The

Analyzing the switching function led to the following statements:

- If  $S \gg K_{hyds}$ ,  $F_{accessibility} \rightarrow 0$  (strict sequential concept, high limitation level)
- If  $S \sim K_{hvds}$ ,  $F_{accessibility} \rightarrow 0.5$

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• If  $S \ll K_{hyd_S}$ ,  $F_{accessibility} \rightarrow 1$  (no limitation)

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$$\rho_i = K_{kyd} S_i \times \frac{S_i/X_i}{K_{S_i} + S_i/X_i} \times X_i \times F_{accessibility_i}$$
 Equation 1

328 If 
$$i = 1$$
,  $S = X_{RC}$  and  $F_{accessibility} = 1$ 

329 If 
$$i = 2$$
,  $S = X_{MC}$  and  $F_{accessibility} = \frac{1}{1 + \frac{X_{RC}}{K_{I,X_{RC}}}}$  Equation 2

330 If i = 3, S = X<sub>SC</sub> and 
$$F_{accessibility} = \frac{1}{1 + \frac{X_{MC}}{K_{I,X_{MC}}}}$$
 Equation 3

331 If i = 4, S = 
$$X_{NE}$$
 and  $F_{accessibility} = \frac{1}{1 + X_{SC}/K_{I\_X_{SC}}}$  Equation 4

- 332 where:
- S is the concentration of organic matter contained in the fraction considered (kg COD/m<sup>3</sup>)
- 334  $K_{hyd}$ S<sub>i</sub> is the growth rate of hydrolytic bacteria for the fraction S<sub>i</sub> (d<sup>-1</sup>)
- 335 Ks is the half-saturation coefficient of hydrolytic bacteria (-)
- $X_i$  is the hydrolytic biomass of each fraction (kg COD/m<sup>3</sup>)
- Faccessibility is a switching function based on the accessibility degree of the substrate (-)
- 338 K<sub>I</sub>S<sub>i</sub> is the switching concentration from one fraction to another in the switching function (kg
- 339  $COD/m^3$ ).
- The biodegradability of each fraction was obtained using the FlashBMP® analysis (Lesteur et
- al., 2011) for the batch tests. In the case of the semi-continuous test with sludge, Jimenez et
- al. (2015a) data were used. The biodegradable fractions as a percentage were calculated using
- each fraction mass balance between feedstock fractionation and digestate fractionation. The
- results allowed the calculation of the biodegradability percentage of each fraction, and thus,
- the inert percentage (i.e. parameters  $f_{X_{RC}}xI$ ,  $f_{X_{MC}}xI$ ,  $f_{X_{SC}}xI$ ,  $f_{X_{NE}}xI$ ).
- 346 The initial values of the state variables (i.e. microorganisms' state variables) used in the
- model were determined by simulating the model under continuous conditions to reach steady-
- 348 state equilibrium. The steady-state values of the state variables were then used as state
- variable initial values. This estimation was considered as a non-linear problem. Using the

modified ADM1, the hydrolysis parameters were optimised by trial and error to minimize the squared value of the difference between predicted and experimental methane production curves.

#### 3. Results and discussion

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3.1. Fraction biodegradability test: case studies on apple, wastewater treatment sludge and wheat straw

In order to test a wide range of molecular and accessibility structures, three substrates were chosen: wheat straw (lignocellulose), apple (i.e. carbohydrates) and wastewater sludge (proteins). Indeed, the lignin protection layer from wheat straw, the floc structure from wastewater sludge and the simpler structure of apple's carbohydrates have specific characteristics to investigate the simultaneous and sequential biodegradation concepts. To reach this goal, the removal of X<sub>RC</sub> and X<sub>MC</sub> fraction (i.e. protection layers) was proposed to investigate the BMP kinetics of total and residual fractions. As shown by Jimenez et al. (2014), the  $X_{RC}$  extractions did not alter the chemical structure of the residual fractions. The substrates fractionations are presented in Figure 3. The BMP tests results are presented in Figure 4. Regarding the accessibility characterization, the method was repeatable as suggested by the standard deviations obtained (less than 5% for  $X_{RC}$  and  $X_{MC}$  and between 3 and 10% for X<sub>SC</sub>). The results are consistent considering the fruits/vegetables, wheat straw and wastewater treatment sludge nature. Indeed, apple contained mainly accessible fractions (large fraction of X<sub>RC</sub>, 68% of COD) while wheat straw is mainly composed of poorly accessible fractions (i.e.  $X_{SC} + X_{NE} = 73\%$  of COD).. The wastewater treatment sludge had intermediate values ( $X_{RC} = 29\%$  and  $X_{MC} = 37\%$  of COD). The saline and basic extractions allowed the ionisation of some poorly attached proteins. This extraction was based on sludge exo-polymeric substance extraction and on the flocs structure of activated sludge (Jimenez et al., 2014), which is why wastewater sludge was mainly composed of X<sub>RC</sub> and X<sub>MC</sub> fractions

(Figure 3). On the contrary, wheat straw contained more fibers such as celluloses, extracted by acid hydrolysis ( $X_{SC}$  fraction).  $X_{NE}$  was mainly composed of non-soluble lignin (Jimenez et al., 2015a). However, some lignin can be solubilised under basic conditions (Carrere et al., 2010). Wheat straw's  $X_{MC}$  fraction contained alkaline soluble lignin. On the contrary, substrate like apple was mainly composed of  $X_{RC}$  fraction, related to soluble sugar and protein. As stated by Jimenez et al (2015b), these results confirmed the ability of the extraction procedure to characterize accessibility and biochemical nature of the substrates.

For each substrate, three BMP tests associated with the biodegradation of the entire substrate, the substrate deprived of  $X_{RC}$  fraction, and the substrate deprived of  $X_{RC}$  and  $X_{MC}$  fractions, after saline and basic extractions respectively were done.

Regarding the cumulated methane production obtained for the apple (Figure 4a), the biodegradability decreased as the accessibility decreased, similar to the rate of each remaining samples after sequential extractions. Both methane production rate and yield values were higher for the total sample than for total sample without  $X_{RC}$  and without  $X_{RC}$  and  $X_{MC}$ . The methane production rate evolution of each fraction could be obtained by subtraction and the simultaneous concept can be applied.

Concerning the wheat straw (Figure 4b), as previously mentioned, the  $X_{RC}$  fraction was low, thus the biodegradability curves of total substrate and of total substrate minus  $X_{RC}$  were very similar. However, when the BMP test was performed on the  $X_{SC}$ +  $X_{NE}$  fractions only, the rate increased (linear curve slope between 1 and 3 days calculated: 46 mlCH<sub>4</sub>·gCOD<sup>-1</sup>·d<sup>-1</sup>) compared to the total substrate without  $X_{RC}$  (linear curve slope between 1 and 3 days calculated: 25 mlCH<sub>4</sub>·gCOD<sup>-1</sup>·d<sup>-1</sup>). Finally, the specific methane productions were the same for the three experiments.

Methane production rate curves from the individual fractions  $X_{RC}$  and  $X_{MC}$  can be calculated according their fractionation percentage of COD in the substrate as explained by Equations 5 and 6.

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$$BMP_{(X_{RC})} = BMP_{(X_{RC} + X_{MC} + X_{SC} + X_{NE})} - BMP_{(X_{MC} + X_{SC} + X_{NE})} \times \frac{x_{MC} + x_{SC} + x_{NE}}{x_{RC} + x_{MC} + x_{SC} + x_{NE}}$$
 Equation 5

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$$BMP_{(X_{MC})} = BMP_{(X_{MC} + X_{SC} + X_{NE})} \times \frac{x_{MC} + x_{SC} + x_{NE}}{x_{RC} + x_{MC} + x_{SC} + x_{NE}} - BMP_{(X_{SC} + X_{NE})} \times \frac{x_{SC} + x_{NE}}{x_{RC} + x_{MC} + x_{SC} + x_{NE}}$$
 Equation 6

- where BMP (X) is the cumulative methane production of the X fraction (NmL  $CH_4$ ) and  $X_{RC}$ ,
- 406  $X_{MC}$ ,  $X_{SC}$ ,  $X_{NE}$  the COD concentration of each fraction (kg COD.m<sup>-3</sup>)

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Figure 5a shows the results obtained after applying Equations 5 and 6 on the wheat straw methane production cumulated curves. The simultaneous hypothesis requires that all the fractions are hydrolysed at the same time (as shown by the Figure 1). In this hypothesis, methane production rate curve associated to X<sub>MC</sub> was calculated and negative values were obtained (Figure 5a), proving that simultaneous hypothesis did not fit. If positive X<sub>MC</sub> methane production rate curve is to be obtained, another approach could be to assume that a fraction n is not hydrolysed until the fraction n-1 reaches low concentrations. This second scenario was simulated using sequential modelling approach and with the switching function previously described (Figure 5b). In the case of the sequential hypothesis, X<sub>MC</sub> is always positive. Therefore, the proposed switching functions (Equations 2 and 3) have to be used for modelling the hydrolysis of each fraction when applying this hypothesis. Overall, the sequential approach is applicable for the three substrates biodegradation. Indeed, the composition and structural accessibility feature of wheat straw and sewage sludge seemed to reveal the sequential concept. Wheat straw and sewage sludge have different physical accessibility structures. Regarding wheat straw, a compact layer of wax covered the outside of the straw, which protects the straw from insects and microorganisms. At the boundary of the primary and second walls a network structure appeard, made of cellulose and hemicellulose,

with some lignin localised on the surface of the network as observed by atomic force microscopy (Yan et al., 2004). Thus, the wheat straw has a lignin and wax layer which makes not accessible a part of cellulose and hemicellulose and the sewage sludge contains exocellular-polymeric substances which were probably extracted and made accessible by alkali extraction. Moreover, the alkaline X<sub>MC</sub> extraction step acts as a pre-treatment for both substrates. It allows the partial solubilisation of recalcitrant material wheat straw. Plant stems have a recalcitrant shell which protects the degradable interior. Alkali treatments induce depolymerisation and cleavage of lignin-carbohydrates linkages (Zhen et al., 2017). In the case of wheat straw, the wax layer protects another layer containing cellulose and pectin (pectin is water soluble). The X<sub>MC</sub> extraction removes the wax layer and allows a quicker biodegradation of the X<sub>SC</sub> fraction (i.e. hemicellulose and cellulose). This means that the poor accessibility of X<sub>SC</sub> limits hydrolysis despite the high biodegradable potential of X<sub>SC</sub> which is consistent with the sequential concept. Similar results were obtained by Rincker et al. (2013) after pre-treatments applied on lignocellulose-like substrates. According to the authors, the lag phase could correspond to a colonisation process. This colonisation phase was also observed for cellulosic fibres with low lignin content (toilet paper) found in primary sludge (Ginestet et al., 2001). In the case of the apple, this phenomenon is not occurring because the fruit was pulped before feeding the reactor and physical structure is lost in the crushed apple. Regarding the sewage sludge (Figure 4c), similar results were obtained as wheat straw. Biological sludge is organized in flocs with cells coated with exo-polymeric substances. This three-dimensional gel-like biopolymer provides protective shielding and prevents cell rupture and lysis influencing flocculation and dewaterability. The cell membranes are also composed of glycan strands crosslinked by peptides acting as barriers to anaerobic digestion (Zhen et al.,

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2017). After X<sub>MC</sub> removal, the flocs were disrupted. Sequential hypothesis fits better than 449 450 simultaneous hypothesis (i.e. negative results obtained, as for wheat straw). The methane production rate slowed down at day 6 (Figure 4) before increasing at day 12. 451 Yasui et al. (2008), Mottet et al. (2013) and Jimenez et al. (2014) also observed such a 452 deceleration phenomenon between readily and slowly biodegraded fractions of organic matter 453 from primary and biological sludge. As no inhibition phenomenon was noticed, the authors 454 455 proposed to use this observation to assess both readily and slowly biodegradable fractions. These results showed that sequential biodegradation concept could be revealed in cases where 456 the accessibility was limited like wheat straw and biological sludge. In those cases, a part of 457 458 X<sub>MC</sub> fraction has to be degraded before to have access to the X<sub>SC</sub> fraction. However, some aspects have to be investigated such as the impact of the chemical extraction procedure on the 459 molecular structure of X<sub>SC</sub>. Even if the lignin barrier of the wheat straw was solubilised by the 460 461 alkaline extraction, one issue not solved was about the initial molecular structure of X<sub>SC</sub> alteration by alkaline extraction. Jimenez et al. (2014) compared the methane production rate 462 curves obtained with whole wastewater treatment sludge and with the sludge after saline + 463 alkaline extraction (10mM). The results showed that the methane production rate curve of the 464 remained pellet overlaid the least biodegradable fraction observed for the whole substrate. 465 466 This means that the  $X_{RC}$  extraction seemed not to alter the  $X_{SC}$  fraction degradation kinetics. However, despite the fact that alkaline condition targets lignin whereas acid condition targets 467 holocelluloses, no similar test has been performed after stronger alkaline extraction. 468 In the apple case, the  $X_{SC}$  biodegradation kinetics was below than those of  $X_{MC}$  and  $X_{RC}$ . It 469 seems that there was no structural accessibility limitation as for wheat straw. Thus, both 470 sequential and simultaneous concepts fit. 471

Based on these results, other substrates were characterized in terms of sequential chemical extraction and anaerobic incubation tests to test the two hypotheses (i.e. simultaneous versus sequential) by comparing the two associated modified models.

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#### 3.2. Results obtained on several substrates

Five substrates were tested with the successive batch test method. They represent a large range of biochemical characteristics as shown by the measured parameters and variables in Table 1. Results of biogas production measured during these batch tests are summarised in Figure 6. Simulations obtained with the simultaneous (i.e. the switching function equal to 1 in the model) and sequential models are also presented in Figure 6. Table 1 presents the measured parameters and variables used in the models and the calibration data parameters, all others parameters of ADM1 being equal to their standard values from Batstone et al. (2002). Fractions and stoichiometric parameters were measured as described in material and methods. The hydrolytic biomass growth rate from sequential and simultaneous kinetics and the switching function parameter value were calibrated using the cumulated methane production rate by trial and error methodology. Table 2 presents the simulated methane production rate vs experimental data errors. The sum of squared errors J can be used as a criterion (Dochain et al., 2001) to calibrate the model and estimate the prediction model quality. From the results obtained, the J values were always lower in the sequential model in comparison with the simultaneous model for the 5 substrates considered. During calibration step of methane production rate, the lowest errors were obtained with switching function parameter K<sub>I\_XRC or XMC</sub> values equal to 0.05 g.m<sup>-3</sup> except for carrot (0.01 g.m<sup>-3</sup>). These values were low compared to the substrates fractions concentrations meaning that the sequential approach limitation was high (i.e. switching function low).

Concerning the potato biodegradation (Figure 6e), both models did not perfectly fit with the experimental behaviour. However, the sequential model gave less error than the simultaneous model. Consequently, the use of the sequential concept for all substrates would be applied to all the substrates to reach a better fit of all methane production rate curves.

## 3.3.Potentials and limitations of the sequential approach

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The sequential chemical extraction methodology was successfully used to simulate bioaccessibility in this study as in previous studies (Jimenez et al., 2014, Jimenez et al., 2015a and b). Jimenez et al. (2014) used the fractionation combined with 3D fluorescence spectroscopy to predict readily and slowly hydrolysable fractions of wastewater treatment sludge. Indeed, the authors showed that the first extractions were associated to the readily hydrolysable fractions whereas the poorly extractible fractions were associated to the slowly hydrolysable fraction. Spectroscopy was used to describe the complexity of each fraction in terms of non-biodegradable molecules. To go further on organic matter biodegradation modelling, this study used the sequential aspect of the protocol to challenge the simultaneous hydrolysis concept and to propose an alternative. The biodegradability study on three substrates after each extraction step revealed that (i) the decrease of accessibility led to a decrease of biodegradability and (ii) the alkaline extraction of two substrates led to an increase of the remaining fraction. Indeed, this extraction can act as a pre-treatment (Carrere et al., 2010). It can solubilise bounded proteins, lipids and lignin. Thus, the protection layer of the wheat straw made of wax and lignin could be solubilised and the flocs from wastewater treatment sludge could be disrupted. According to these results, we hypothesized that the protection structure of both substrates led to reveal the sequential approach. Indeed, X<sub>SC</sub> evolution kinetics was then calculated. Negative values were obtained showing that simultaneous approach could not fit the data. However, the impact of chemical extraction on the molecular structure of the remaining fraction was not evaluated.

Moreover, the chemical extraction procedure applied seemed to not alter the bioaccessibility of X<sub>MC</sub> components after the first alkaline extraction as shown (Jimenez et al., 2014). However, this statement was not proven for X<sub>SC</sub> and X<sub>NE</sub> fractions. After strong alkaline and acid extractions, the molecular structure could indeed be altered, affecting the sequential model parameters. This issue could be a limitation of the use of this technique to represent the reality and should be deeply investigated. More generally, the introduced switching function decreased the errors between experimental and simulated data on methane production curves for all the studied substrates. However, this function consists on a limitation concept that relies on a specific concentration of the considered variable. When the concentration is above the calibrated K<sub>L</sub>X parameter value, sequential degradation occurs and only the first accessible fraction is degraded. Then, the value becomes equal to or below the calibrated K<sub>I</sub> X parameter value. In this case, the next accessible fraction begins to be degraded and the model leads to a simultaneous degradation model. Does this mean that hydrolysis is a mixture of sequential and simultaneous processes as suggested by Morgenroth et al. (2002)? Clearly more in-depth research is required to answer this.

# 4. Conclusions

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The objective of this paper was to use an organic matter characterization method based on accessibility assessment to compare two hydrolysis modelling concepts: simultaneous versus sequential degradation. This comparison revealed that the sequential hydrolysis concept is applicable to all the substrates studied (protein-like and carbohydrates to fibrous-like substrates). The simultaneous model scenario did not fit to all the experimental curves of methane production as highlighted by the study of wastewater treatment sludge and wheat straw biodegradation. However, some issues about the experimental fractionation methodology and its impact on fraction biodegradation kinetics, and on calibrated model

parameters values have been raised. Further investigation on this topic should be done to

validate the proposed model.

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# Simultaneous concept

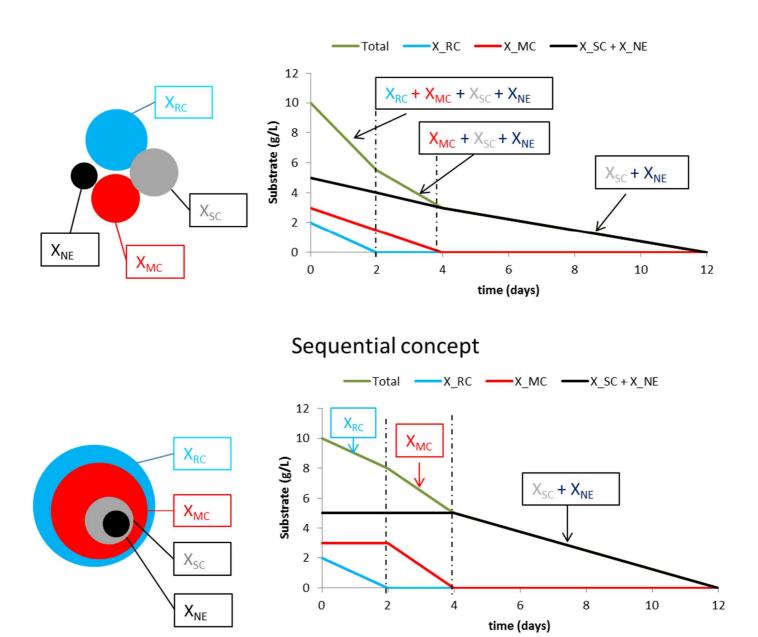


Figure 2: Schematic definition of simultaneous and sequential concepts

Legend: readily hydrolysable fractions  $(X_{RC})$ , moderately hydrolysable  $(X_{MC})$ , slowly hydrolysable fractions  $(X_{SC})$  and poorly hydrolysable fractions  $(X_{NE})$ 

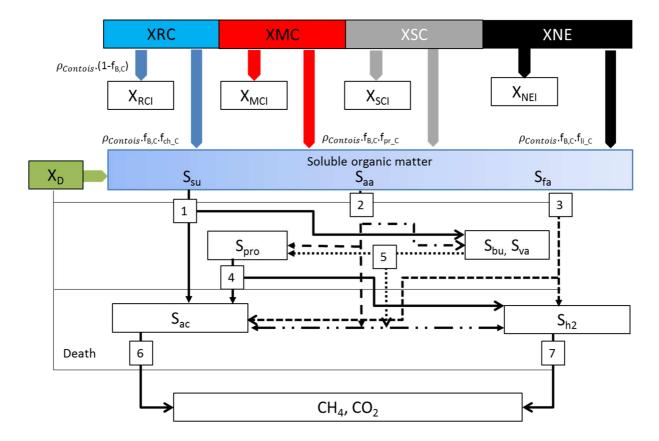


Figure 2: Modified ADM1 model proposed, (1) acidogenesis from sugars, (2) acidogenesis from amino acids, (3) acetogenesis from long chain fatty acids, (4) acetogenesis from propionate, (5) acetogenesis from butyrate and valerate, (6) acetoclastic methanogenesis and (7) hydrogenotrophic methanogenesis. Schematic overview of the modified anaerobic digestion model based on ADM1

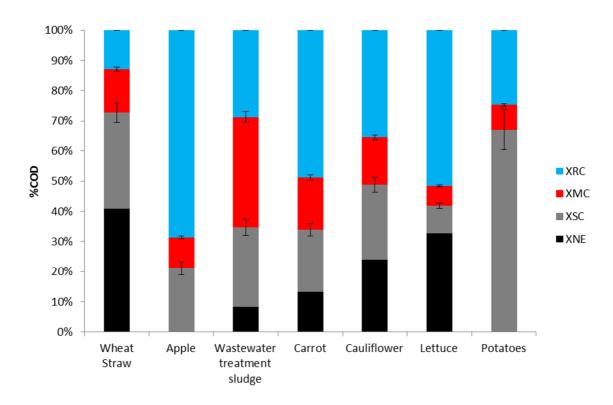


Figure 3 : COD fractionation of the studied substrates

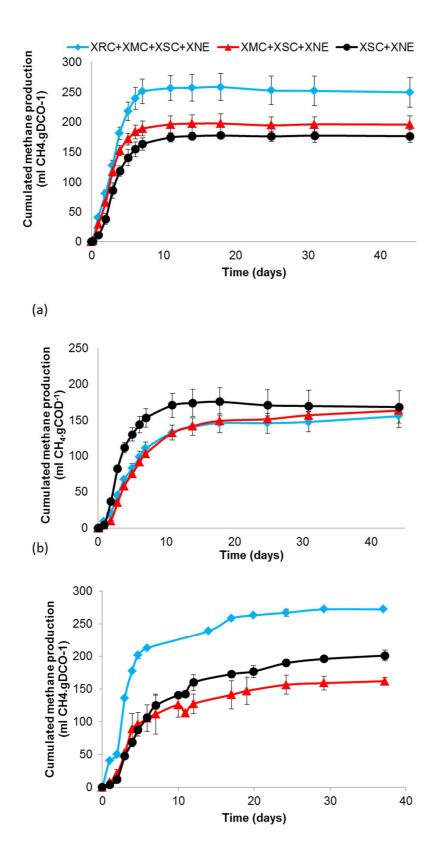


Figure 4: Anaerobic biodegradation of the apple (a), the wheat straw (b) and the wastewater treatment sludge fractions (c)

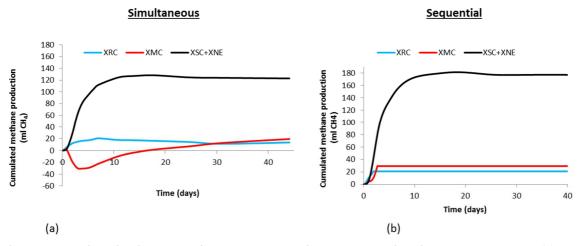


Figure 5: Fraction kinetics calculation based on experimental data using simultaneous concept (a) and fraction kinetic simulation based on sequential concept model (b) of the digestion of wheat

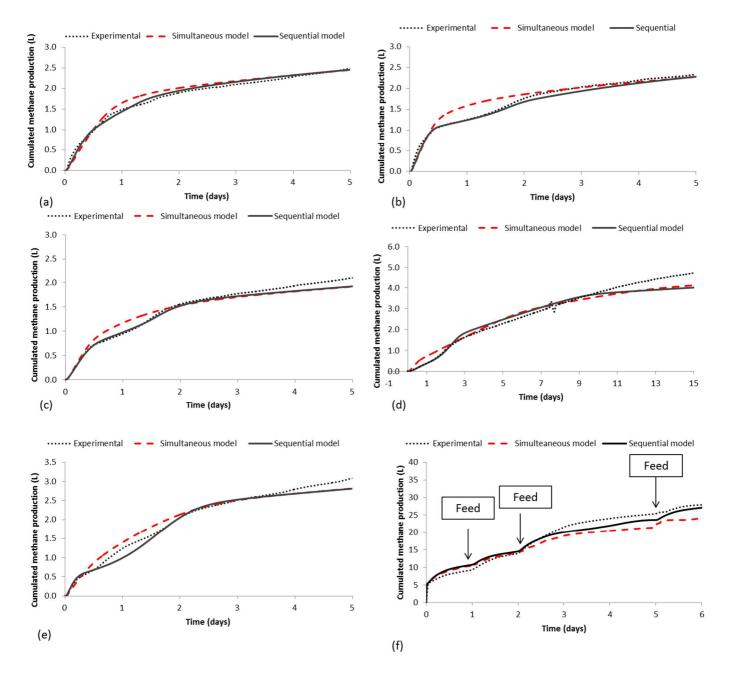


Figure 6: Cumulated methane production curves obtained experimentally (black dot line) and by simulations with the simultaneous model (red dashed lines) and with the sequential model (black line) (a: carrot, b: cauliflower, c: lettuce, d: wheat straw, e: potato and f: wastewater treatment sludge)

Table 1 : Calibration parameters of simultaneous and sequential model for the five substrates

				Carrot	Cauliflower	Lettuce	Wheat straw	Potato	Wastewater treatment sludge
ameters	<u>.</u> . E		X <sub>RC</sub>	0.59	0.47	0.63	0.51	0.33	0.29
	COD per fraction (kgDCO.m	$X_{MC}$	0.21	0.21	0.08	0.56	0.11	0.37	
		$X_{SC}$	0.25	0.33	0.11	1.26	0.90	0.26	
	<b>5</b> *** <b>3</b>		$X_{NE}$	0.16	0.32	0.40	1.61	0.00	0.08
			f_XRC_xI	0.00	0.20	0.24	0.51	0.00	0.21
		rt, proteins, (%COD)		0.73	0.55	0.37	0.02	0.77	0.19
l pu				0.05	0.19	0.09	0.04	0.23	0.46
es a				0.22	0.01	0.18	0.43	0.00	0.14
able				0.21	0.70	0.66	0.80	0.19	0.65
/ari		o inc	f_XMC_ch	0.31	0.16	0.03	0.06	0.19	0.08
Measured variables and parameters	Fractions content into inert, proteins, lipids and carbohydrates (%COD)		f_XMC_pr	0.05	0.13	0.03	0.02	0.00	0.20
			f_XMC_li	0.43	0.01	0.28	0.12	0.62	0.07
			f_XSC,NE_xI	0.43	0.18	0.42	0.46	0.03	0.80
			f_XSC,NE_ch	0.33	0.52	0.17	0.40	0.79	0.18
			f_XSC,NE_pr	0.01	0.14	0.06	0.01	0.01	0.02
			f_XSC,NE_li	0.23	0.16	0.35	0.13	0.17	0
leters	Experimental data used		BMP 2.0	BMP 2.0	BMP 2.0	BMP 2.0	BMP 2.0	Fed batch reactor	
	Switch (kg.COD.m <sup>-3</sup> )  Sequential Kinetics (d <sup>-1</sup> )		K <sub>I</sub>	0.01	0.05	0.05	0.05	0.05	0.05
			Khyd_XRC	3.50	4.00	4.00	10.00	5.00	11
ran_		Kinetics (d <sup>-1</sup> )	Khyd_XMC	2.50	2.00	1.00	3.50	1.00	9
Calibrated parameters			Khyd_XSC	2.50	1.00	9.00	3.50	1.50	9
			Khyd_XNE	0.50	0.50	7.00	0.80	0.50	9
	Simultaneous kinetics (d-1)  Khyd_XRC  Khyd_XMC  Khyd_XSC  Khyd_XNE		2.00	4.00	4.00	5.00	2.00	9	
			Khyd_XMC	1.67	2.00	2.00	0.50	1.00	6
			Khyd_XSC	1.67	1.00	1.00	0.80	0.75	6
			Khyd_XNE	0.33	0.50	1.00	0.50	0.25	6

Table 2: Estimation of the quality of each model by the the sum of squared errors

	N	J	J
		simultaneous	sequential
		model	model
	5219	58	15
Carrot			
	5001	93	75
Potato			
	4999	124	23
Cauliflower			
	5219	78	35
Lettuce			
Wheat	5000	182	97
Straw			
Wastewater			
treatment	145	955	309
sludge			

J is the sum of squared errors and N the number of data points to fit